

TABLE 3. CORRECTION FACTORS FOR DIRECT CAST-IRON RADIATORS AND CONVECTORS*

STEAM PRESS. APPROX.	HEATING MEDIUM TEMP F	FACTORS FOR DIRECT CAST-IRON RADIATORS								FACTORS FOR CONVECTORS							
		ROOM TEMPERATURE F								INLET AIR TEMPERATURE F							
		80 75 70 65 60 55 50								80 75 70 65 60 55 50							
Gage Vacuum In. Hg.	Abs. Lb per Sq In.	150	160	170	180	190	200	210	220	230	240	250	260	270	280	290	300
22.4	3.7	150	2.58	2.36	2.17	2.00	1.86	1.73	1.62	3.14	2.83	2.57	2.35	2.15	1.98	1.84	1.71
20.3	4.7	160	2.17	2.00	1.86	1.73	1.62	1.52	1.44	2.57	2.35	2.15	1.98	1.84	1.71	1.59	1.49
17.7	6.0	170	1.86	1.73	1.62	1.52	1.44	1.35	1.28	2.15	1.98	1.84	1.71	1.59	1.49	1.40	1.32
14.6	7.5	180	1.62	1.52	1.44	1.35	1.28	1.21	1.15	1.84	1.71	1.59	1.49	1.40	1.32	1.24	1.17
10.9	9.3	190	1.44	1.35	1.28	1.21	1.15	1.10	1.05	1.59	1.49	1.40	1.32	1.24	1.17	1.11	1.05
6.5	11.5	200	1.28	1.21	1.15	1.10	1.05	1.00	0.96	1.40	1.32	1.24	1.17	1.11	1.05	1.00	0.95
Lb per Sq In.																	
1	15.6	215	1.10	1.05	1.00	0.96	0.92	0.88	0.85	1.17	1.11	1.05	1.00	0.95	0.91	0.87	0.83
6	21	230	0.96	0.92	0.88	0.85	0.81	0.78	0.76	1.00	0.95	0.91	0.87	0.83	0.79	0.76	0.72
15	30	250	0.81	0.78	0.76	0.73	0.70	0.68	0.66	0.83	0.79	0.76	0.73	0.70	0.68	0.65	0.63
27	42	270	0.70	0.68	0.66	0.64	0.62	0.60	0.58	0.70	0.68	0.65	0.63	0.60	0.58	0.56	0.54
52	67	300	0.58	0.57	0.55	0.53	0.52	0.51	0.49	0.56	0.54	0.53	0.51	0.49	0.48	0.47	0.45

*To determine the size of a radiator or a convactor for a given space, divide the heat loss in Btu per hour by 240 and multiply the result by the proper factor from the above table.

To determine the heating capacity of a radiator or a convactor under conditions other than the basic ones with the heating medium at a temperature of 215 F, and the room temperature at 70 F in the case of a radiator, and the inlet air temperature at 65 F in the case of a convactor, divide the heating capacities at the basic conditions by the proper factor from the above table.

rating-test conditions to output under other operating conditions. Such factors are given in Table 3.

When it is desired to change the output under any test conditions to the corresponding output under standard Code test conditions, the reciprocal form of correction factor may be derived. The equations for steam units are:

For radiators:

$$C_s = \left(\frac{215 - 70}{t_s - t_r} \right)^{1.3} \quad (1)$$

For convectors:

$$C_s = \left(\frac{215 - 65}{t_s - t_i} \right)^{1.5} \quad (2)$$

The output under standard conditions will be:

$$H_s = C_s H_t \quad (3)$$

where

C_s = correction factor.

t_s = steam temperature during test, Fahrenheit degrees.

t_r = room temperature during test, Fahrenheit degrees.

t_i = inlet air temperature during test, Fahrenheit degrees.

H_s = heat emission rating under standard conditions, Btu per hour.

H_t = heat output under test conditions, Btu per hour.

The relation between the size of the radiator or convactor and the size of the test room will affect the results obtained in a capacity-rating test. The height and location of the radiator and the insulation of the test room are other important factors that are not specifically regulated by the Code.

For a radiator, the finish coat of paint affects the heat output. Oil paints of any color will give about the same results as unpainted black or rusty surfaces, but an aluminum or a bronze paint will reduce the heat emitted by radiation. The net effect may be a reduction of 10 per cent or more in the total heat output of the radiator.^{6,6,7}

Radiator enclosures and convactor casings affect the heat distribution within the room as well as the total amount of heat supplied by the steam or hot water.⁸

Heating Effect

For several years the term *heating effect* has been used to designate the relation between the *useful output* of a radiator, in the comfort zone of a room, and the total input as measured by steam condensation or water temperatures^{9,10}. The application of such a heating effect factor is a recognition that some radiators and convectors use less steam than others for producing equal comfort heating results in the room.

No standard method for evaluating the heating effect of radiators and convectors and correlating it with comfort has yet been accepted. One method, with test data¹¹ on radiators and convectors, and making use of the eupatheoscope for evaluating the environment produced, has been suggested by the University of Illinois. The principle underlying the eupatheoscope involves the measurement of the heat loss from a sizable

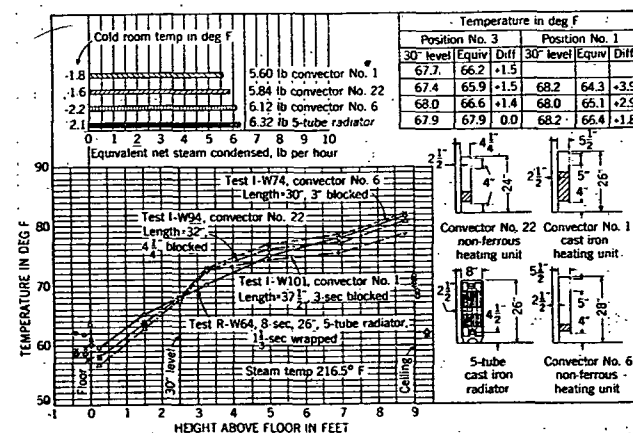


FIG. 2. TEMPERATURE GRADIENTS AND EQUIVALENT TEMPERATURES FOR RADIATOR AND CONVECTORS WITH COMMON 30 IN. LEVEL TEMPERATURE

body by radiation and convection, when the surface is maintained at some constant temperature. Through the use of this instrument and its calibration curve, non-uniform environments may be referred to uniform environments in which the air and all surrounding surfaces are at the same temperature. The temperatures of the uniform environments are referred to as equivalent temperatures.

The Kata thermometer¹², the thermo-integrator^{13,14}, and the globe¹⁵ thermometer are other instruments which have been used to measure the influence of air temperature, air movement and radiation in an environment.

Data given in Fig. 2 show that while the air temperature at the 30-in. level is the same for the three convectors and the one large-tube cast-iron radiator, in position No. 3 in the test room, the equivalent temperature is 1.5 F lower than the air temperature in the case of the three convectors, and the same as the air temperature in the case of the radiator. The difference between the minimum and the maximum amount of heat