



Region 6 - Enforcement & Compliance Assurance Division
INSPECTION REPORT

Inspection Date(s):	08/04/2022	
Media Program:	Air	
Regulatory Program(s)	Title V CAA	
Company Name:	Louisiana Integrated Polyethylene JV, LLC	
Facility Name:	Louisiana Integrated Polyethylene JV	
Facility Physical Location:	2201 Old Spanish Trail	
(city, state, zip code)	Westlake, LA 70669	
County/Parish:	Calcasieu	
Facility Coordinates	30.24502, -93.27563	
Facility Phone Number:		
Facility Contact:	Megan Leger	Environmental Manager
	Megan.leger@lyondellbasell.com	
FRS Number:	110070879384	
Identification/Permit Number:	LDEQ AI 226602	
Media Identifier Number:	LA0000002201900514	
NAICS:	325110	
SIC:	N/A	
Personnel participating in inspection:		
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Dan Hoyt	EPA OECA, Air Enforcement Division	Environmental Engineer
Jon Morris	Providence Photonics	EPA Contractor
Michael Morris	Providence Photonics	EPA Contractor
Megan Leger	Louisiana Integrated Polyethylene JV	Environmental Manager
Beau Mixon	Louisiana Integrated Polyethylene JV	Environmental Engineer
Ashton Singletary	Louisiana Integrated Polyethylene JV	Environmental Engineer
EPA Lead Inspector Signature/Date		
	James Haynes	Date
Supervisor Signature/Date		
	James Leathers	Date

Section I – INTRODUCTION**PURPOSE OF THE INSPECTION**

I, James Haynes, U.S. Environmental Protection Agency (“EPA”) Region 6 inspector, arrived at the Louisiana Integrated Polyethylene Joint Venture (“LIP JV”) in Westlake, Louisiana on August 4, 2022, to conduct an unannounced Clean Air Act (“CAA”) inspection. I arrived with Ms. Colleen McCarthy, EPA Region 6 inspector, Mr. Dan Hoyt, EPA OECA-AED inspector, and two EPA contractors with Providence Photonics – Mr. Jon Morris and Mr. Michael Morris. We met with LIP JV representatives Ms. Megan Leger, Environmental Manager; Ms. Ashton Singletary, Environmental Engineer; and Mr. Beau Mixon, Environmental Engineer. I presented my inspector credentials to Ms. Leger and notified her of our intent to conduct a CAA Partial Compliance Evaluation (“PCE”). EPA contracted Providence Photonics to conduct flare observations using the Video Imaging Spectral Radiometry (“VISR”) method. The VISR method uses a multi-spectral mid-wave infrared imager to measure relative concentrations of combustion gases to calculate flare combustion efficiency.

FACILITY DESCRIPTION

The LIP JV facility is in Westlake, Louisiana near the Calcasieu River located at 2201 Old Spanish Trail, Westlake, Louisiana 70669. The facility encompasses approximately 405 acres and was founded as a joint venture between Sasol Chemicals LLC and LyondellBasell Industries N.V. in December 2020. The facility operates 8760 hours per year with 434 full time staff and approximately 470 contractors. The facility is comprised of the Low Density Polyethylene (“LDPE”) and Linear-Low Density Polyethylene (“LLDPE”) units, Ethylene 2 unit, a Steam 2 Unit, the Utilities, Offsite, and Infrastructure (“UO&I”) unit, and the Wastewater Treatment Plant 2 (“WWTP2”). The WWTP2 receives wastewater from the Sasol Chemicals Complex’s Ethylene Oxide/Ethylene Glycol (“EO/EG”) unit, Ethoxylation Units (“ETO”) 4 & 5, and the Guerbet Alcohol Unit.

The LDPE, LLDPE, Ethylene 2, Steam 2, UO&I, and WWTP2 units operate under individual CAA Title V permits. The facility operates three ground flares (One for the Ethylene 2, LLDPE, and LDPE units) and one elevated flare (UO&I units).

Section II – OBSERVATIONS

After entry, Ms. Leger provided me with an overview of the site operations and current conditions. Ms. Leger stated the facility has three ground flares and one elevated flare. Providence Photonics set up the imaging device outside the process area and began collecting data at the elevated flare at 5:02 PM. Providence Photonics stopped collecting data at the elevated flare at 5:20 PM. I conducted a brief closing conference with LIP JV, and we exited the facility.

Section III – AREAS OF CONCERN

I observed no areas of concern at the time of inspection.

Section IV – FOLLOW UP

After EPA exited the facility, no additional information was requested or submitted.

Section V – LIST OF APPENDICES

Appendix 1 – VISR Flare Measurement Report

Appendix 1

VISR Flare Measurement Report



VISR Flare Measurement Report

**Facility: Louisiana Integrated
Polyethylene JV**

4101 LA 108

Westlake, LA 70669

Calcasieu Parish, Louisiana

Prepared for
US Environmental Protection Agency
Region 6
1201 Elm Street, Suite 500
Dallas, TX 75270

PROJECT NO. 0010-004-008

PREPARED BY
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Introduction

Through its contract 68HERC21D0007/Task Order 68HERC21F0185 with Eastern Research Group, Inc. (ERG), EPA Office of Enforcement and Compliance (OECA) and Region 6 retained Providence Photonics, LLC (Providence) to assist the inspection of the Louisiana Integrated Polyethylene JV (LIP) plant located at 4101 Hwy 108, Westlake, Louisiana, 70669. Providence measured the combustion efficiency (CE) and other performance metrics of the flare using the Video Imaging Spectral Radiometry (VISR) method.

Background

The VISR method utilizes a multi-spectral mid-wave infrared imager to remotely and continuously measure relative concentrations of combustion gases. Based on these relative concentrations, flare CE is calculated. The VISR method provides continuous measurement of the following five flare performance metrics at 1-second data rate.

1. **Combustion Efficiency (0 to 100%):** Combustion efficiency (**CE**) is a measure of the relative concentration of hydrocarbon vs. carbon dioxide in the post combustion gas plume. If there is no hydrocarbon present in the post combustion gas plume, then CE is 100%.
2. **Smoke Index (0 to 10):** Smoke index (**SI**) is a unit-less number which indicates the degree of visible emissions within the combustion envelope. A SI of 0 means no visible emissions are present while a SI of 10 means the flare has heavy black smoke. While SI only represents the degree of visible emissions within the combustion envelope, it is generally correlated to opacity and a SI above 3 generally indicates that some visible emissions are likely present outside of the combustion envelope.
3. **Flame Footprint (m²):** Flame footprint (**FF**) is a measure of the flame size in square meters. It is not necessarily correlated to the visible flame size as the FF is determined by the Infrared radiance, not the visible flame. Note that the orientation of the flame will impact the FF as the depth of the flame will change with viewing angle.
4. **Fractional Heat Release (MMBtu/Hr):** Fractional Heat Release (**FH**) is a measure of the heat released from flare combustion in the spectral bands monitored by the Mantis flare monitor. Although it is not a measure of the total heat release across the entire energy spectrum, FH is expected to be correlated to the total heat release.
5. **Flame Stability (0 to 100%):** Flame stability (**FS**) is a measure of the change in radiance measured by the Mantis flare monitor in a 1-second interval. A FS of 100% indicates a flame that has a constant radiance. A low FS value (generally lower than 80%) indicates a flame with significant radiance fluctuation within 1 second interval, suggesting a less stable flame. Variability on a longer time scale will not be described by the flame stability metric.

Appendix B provides additional information on the accuracy and precision of the VISR method. More information about the VISR method and its validation is provided at <https://www.providencephotonics.com/flare-monitoring>.

Summary of Inspection

Inspection Date: August 4th, 2022

Personnel: James Haynes (EPA Region 6) Jon Morris (Providence)
Colleen McCarthy (EPA Region 6) Michael Morris (Providence)
Daniel Hoyt (EPA OECA)

Facility: Louisiana Integrated Polyethylene JV
4101 LA 108, Westlake, LA 70069

Results: **Table 1** below provides a summary of the VISR results. Complete results can be found in **Appendix A**.

Date	Start Time (Local)	End Time (Local)	Site Description	Distance (m)	Temp (°C)	RH (%)	Avg Wind Speed (mph)	CE Avg (%)	SI Avg	FF Avg (m2)	FH Avg (MMBTU/HR)	FS Avg (%)
8/4/2022	5:02 PM	5:20 PM	Steam Assisted	151	30	57	6 - 8	97.51	0.63	55.32	1.12	96.43

Table 1: Summary VISR Results.

Observations

The following sections describe field observations and comparisons derived from the dataset.

Field Conditions

The inspections were conducted on August 4th, 2022. Each measurement with the VISR instrument was within the method limits for distance, as determined by the minimum plume pixels required by the QAPP. The ambient temperature was 30°C and winds were generally moderate, from 6-8 mph. A rain event occurred at the end of the measurement period but did not impact the data quality.

Louisiana Integrated Polyethylene JV Flare

The LIP flare performance data is plotted in **Figures 1 and 2** below. **Figure 1** shows Combustion Efficiency vs. Fractional Heat Release and **Figure 2** shows Combustion Efficiency vs. Smoke Index. There were no visible emissions from this flare, as indicated by the Smoke Index values < 3. Average Combustion Efficiency for this measurement was 97.51% and the average Smoke Index was 0.63.

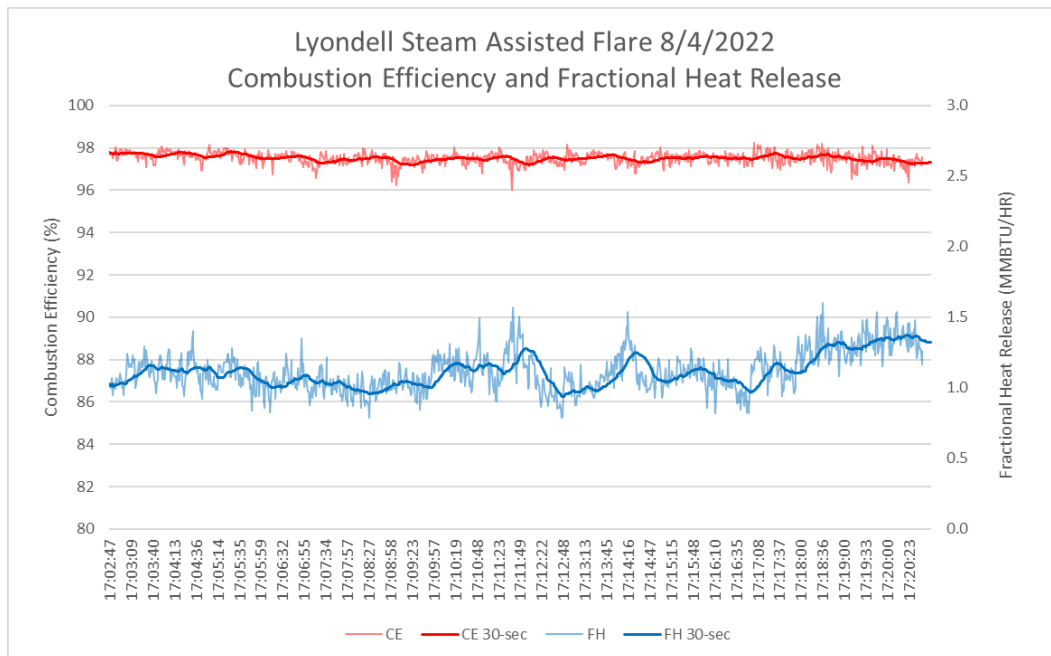


Figure 1: Combustion Efficiency and Fractional Heat Release for the LIP flare on 8/4/2022.

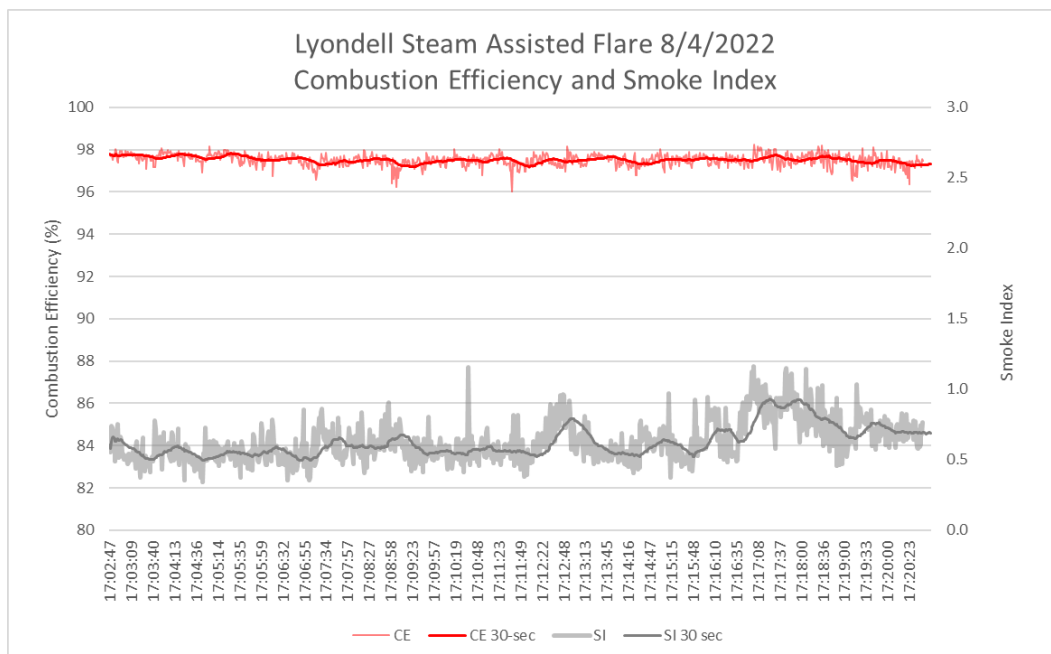


Figure 2: Combustion Efficiency and Smoke Index for the LIP flare on 8/4/2022.

Electronic Data Generated from the Test

The following electronic data are submitted to the US EPA Region 6 as part of this report:

- A Microsoft Excel file containing second-by-second results from the VISR instrument and averages for each measurement period.
- FLIR video recording of each flare during the inspection.

References

1. Yousheng Zeng, Jon Morris & Mark Dombrowski (2015) Validation of a new method for measuring and continuously monitoring the efficiency of industrial flares, Journal of the Air & Waste Management Association, 66:1, 76-86, DOI: [10.1080/10962247.2015.1114045](https://doi.org/10.1080/10962247.2015.1114045)
2. Yousheng Zeng, Jon Morris. (2019, April 2nd). *Precision and Accuracy of the VISR Method for Flare Monitoring*. Air Quality Measurement Methods and Technology, Durham, North Carolina, United States.

Appendix A: Results

Date/Time			Site Description		Conditions				Efficiency (%)				Smoke Index (0-10)				Flare Footprint (m ²)				Fractional Heat (MMBTU/HR)				Flame Stability (%)			
Date	Start Time (CST)	End Time (CST)	Site	Description	Distance (m)	Temp (°C)	RH (%)	Wind Speed (mph)	CE Avg	CE Min	CE Max	SD	Avg	Min	Max	SD	Avg	Min	Max	SD	Avg	Min	Max	SD	Avg	Min	Max	SD
8/4/2022	5:02 PM	5:20 PM	LIP	Steam Assisted	151	30	57	6 - 8	97.51	96.01	98.25	0.28	0.6	0.3	1.2	0.1	55.3	35.9	77.8	7.2	1.118	0.790	1.605	0.141	96.4	55.1	100.0	2.9

Table 2: Complete VISR Results.

Appendix B: Validation of the VISR method

Precision and Accuracy of the VISR Method for Flare Monitoring

Extended Abstract: ME92

Presented at the conference:

Air Quality Measurement Methods and Technology

April 2-4, 2019

Durham, NC

Jon Morris, Yousheng Zeng, and Srikanth Mutyala
Providence Photonics, Baton Rouge, Louisiana

Introduction

Industrial flares represent a large category of air emission sources for Volatile Organic Compounds (VOC), air toxics, and greenhouse gases (GHG)¹⁻⁴. Depending on their combustion efficiency (CE), the emissions of these air pollutants can be significantly different. Despite the large contribution of flares to air emission inventories, flares are the only source category for which no EPA test or monitoring methods can be applied to directly measure their efficiency or emission rates. As a result, flare emissions in air emission inventories may carry significant uncertainties.

A method based on Video Imaging Spectral Radiometry (VISR) has been developed for testing or continuously monitoring combustion efficiency (CE) of industrial flares⁵. To validate the VISR method, tests were conducted at flare test facilities of Zeeco, Inc. (Zeeco) and John Zink Hamworthy Combustion (John Zink), both located in Tulsa, Oklahoma, in September and October 2016, respectively. The test at Zeeco included both an air assisted flare and a steam assisted flare. Twenty-eight flare conditions were tested, 14 for the air flare and 14 for the steam flare. This test is referred to as the "Zeeco Test" in this paper.

The test at John Zink was part of a program sponsored and organized by the Petroleum Environmental Research Forum (PERF), an industry consortium. PERF project 2014-10 Direct Monitoring of Flare Combustion Efficiency was created and funded by participating PERF companies to provide a test platform for various developers/vendors of flare remote sensing technologies (Invitees) to participate in a blind test to evaluate the effectiveness of each technology. The blind test was administered by John Zink. Testing began on October 17th, 2016 and continued for 10 days, concluding on October 27th, 2016. The flare tip used was the John Zink model EEF-QSC-36, which was the same flare tip used during the 2010 TCEQ Flare Study⁴. A test protocol was developed which identified a series of test conditions to evaluate various factors

that could affect flare CE measurement. Only limited logistical and environmental factors were shared with the Invitees (i.e., distance from the flare, view angle with respect to flame orientation due to wind, sun in/out of the field of view, daytime/nighttime testing). Information regarding flare operations such as the type of fuel gas used, firing rates, steam rates or any other flare operating parameters was concealed from Invitees. A total of 45 test points was evaluated over the 10 days of testing. Extractive sampling was performed on each test point as the control method for flare CE measurement. The results of the extractive sampling were not provided to Invitees until Invitees submitted their own results based on their respective measurement technology. This test is referred to as the "PERF Test" in this paper.

In this paper, the precision and accuracy of the VISR method are evaluated based on the test campaigns described above.

Methods and experimental setup

The VISR flare monitor is a remote monitoring device that can be positioned at any distance as long as the flare to be monitored is in the line of sight and there are a sufficient number of pixels of the flare flame image in the VISR monitor. The distances from flare to the VISR monitor in the experiments reported here were in the range of 174 feet to 650 feet. To evaluate the performance of the VISR method, an extractive sampling system was used as a reference method. A sample extraction apparatus was suspended by a crane over the flare plume to extract combustion product gases. The sample was transported through a heated sampling line to a sample manifold in a testing trailer. The sample manifold was connected to analyzers for oxygen (O₂), carbon dioxide (CO₂), carbon monoxide (CO), and hydrocarbon (HC). The methods for measuring O₂, CO₂, CO, and HC were EPA Method 3A, 3A, 10, and 25A, respectively. The level of O₂ was used to confirm that the sampling probe was in the flare plume. The concentrations of CO₂, CO, and HC were used to calculate flare CE per method used in the 2010 TCEQ flare study³.

These test campaigns covered a wide range of process conditions: two steam flares and one air flare; multiple vent gas compositions (natural gas, propane, propylene, hydrogen, in pure form or mixed with nitrogen; vent gas flow range from 10 lb/hr to 10,000 lb/hr; various steam and air assist levels resulting in combustion zone net heating value (NHVcz) in a range of 120 to 1,250 Btu/scf for the steam flares and net heating value dilution parameter (NHVdil) in a range of 6.7 to 244 Btu/ft² for the air flare.

The test campaigns also covered a wide range of environmental conditions: distance ranging from 174 ft. to 650 ft.; different wind speed and direction (crosswind, wind oriented towards VISR device, and wind oriented away from VISR device); daytime vs. nighttime; various sky conditions (blue sky, cloudy, moving clouds); the Sun in or out of field of view; rain, and fog.

Results and Discussions

Precision

Precision is a measure of how the results of multiple measurements by the same method scatter while the target of the measurement holds steady. This is difficult to assess for flare measurements because even when the flare operating conditions are held steady (as they were in each test point of the PERF Test), the flare CE may change due to changes in environmental conditions. Analyte spiking or quadruplet sampling described in EPA Method 301 would help to isolate the measurement method precision from the fluctuation of the target itself⁶. However, these methods are not feasible for flare measurement. Nevertheless, the measurement precision can still be evaluated using the data from the PERF test. For each PERF test condition, 4 segments of measurement were made by the extractive method and 3 segments of measurement were made by VISR while the flare operating conditions were held constant (although flare CE did fluctuate due to changes in environmental conditions). The standard deviation (SD) and relative standard deviation (RSD) can be calculated based on these replicate measurements. **Table 1** is a summary of the SD and RSD for both the VISR method and the extractive method used in the PERF Test. As shown in **Table 1**, the RSD for the VISR method is in a range of 0.07% to 1.98% with an average of 0.62%. The variation of the VISR method appears to be slightly better than the extractive method from the perspective of both the average and the range of the RSD values, suggesting that the precision of VISR is at least as good as the extractive method. Note that in both cases, the variation due to changing environmental conditions is included in the RSD as there is no practical method to separate it. Despite the inclusion of environmental changes, the RSD is more than an order of magnitude smaller than 20% as required in EPA Method 301 (Section 9.0)⁶. If a more stringent criteria is used in which the 20% limit on RSD is applied to the most relevant range of 90-100 % CE measurement (i.e., in the span of 10 % CE measurement), the criteria would be SD < 2 % CE (20% of 10% = 2 % CE). As shown in **Table 1**, the highest SD is 1.84 measured as % CE, which is lower than the SD of 2 % CE measurement and therefore satisfies the more stringent criteria.

Table 1. Relative Standard Deviation (RSD) of VISR and extractive method per PERF Test

Method	CE Avg.	CE Range	SD Avg.	SD Range	RSD Avg.	RSD Range
VISR	96.47	80.61-99.91	0.59	0.07-1.84	0.62%	0.07-1.98%
Extractive	96.41	83.50-100.00	0.83	0.00-2.61	0.88%	0.00-2.72%

The Zeeco Test did not include multiple replicated measurements under each test condition. Therefore, a precision analysis is not performed on that data.

Accuracy

The accuracy of the VISR method is evaluated based on the Zeeco Test and PERF Test. In these two tests, the flare CE was measured by both the VISR method and the extractive method. The extractive method was used as the control (reference) method. Strictly speaking, what can be assessed is the agreement between the two methods, not the accuracy of either method because the true flare CE is unknown. The agreement between the two methods can be evaluated using a statistical method. One such method is to use t-test on the differences between the paired CE measurements by VISR and extractive methods. This method is the same as the method used in EPA Method 301 to determine if there is a difference caused by different sample storage time⁶ (it should be noted that the methods for bias described in Method 301 are not directly applicable because they are specifically designed for analyte/isotopic spiking or quadruplet sampling systems, which are not feasible for flare measurement). The value of the t-statistic is calculated using the following equation.

$$t = \frac{|d_m|}{\frac{SD_d}{\sqrt{n}}}$$

Where d_m and SD_d are the mean and the standard deviation of the difference of the paired samples (VISR and extractive sample), and n is the total number of samples. The resulted t-statistic value is compared to the critical value of the t-statistic with a 95 percent confidence level and $n-1$ degree of freedom. If the resulted t-statistic value is less than the critical value, the difference between the VISR method and the extractive method is not statistically significant, i.e., the two methods are statistically the same. The results of the t-statistical analysis for both Zeeco and PERF tests are summarized in **Table 2**. The number of samples (tests) in **Table 2** is less than the number of tests actually conducted because some tests were designed for other purposes (e.g., smoke test) and they are not included in the evaluation of the agreement between VISR and extractive methods.

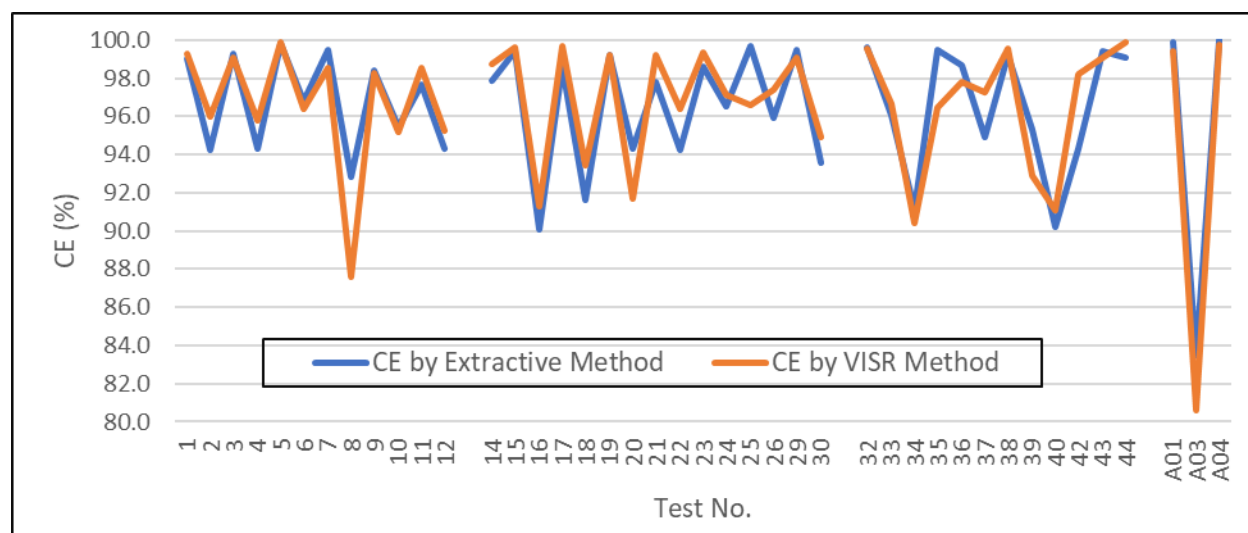
Table 2. t-Test to determine if the VISR method is different from the extractive method

	Zeeco Test (Steam Flare)	Zeeco Test (Air Flare)	PERF Test
No. of Samples, n	11	9	42
Mean Difference, d_m (% CE)	0.30	-0.21	0.07

Standard Deviation, SD_d (% CE)	1.32	0.65	1.69
t-Statistic Value	0.756	0.967	0.254
Degree of Freedom	10	8	41
t ₉₅ Critical Value	2.228	2.306	2.020
Statistically Different?	No	No	No

As demonstrated in **Table 2**, statistically there is no difference between the flare CE measured by the VISR method and by the extractive method. The agreement between the two measurement methods can also be illustrated in **Figure 1** using the results from the PERF Test.

Figure 1. Flare CE measured by VISR method and extractive method – PERF Test results



Conclusion

Industrial flares can now be measured or continuously monitored by the VISR method for their performance, i.e., combustion efficiency (CE). The VISR method is a remote sensing method and can be deployed easily and practically. The VISR method transforms flare testing/monitoring from most difficult task (impossible in many cases) to a task that is easier than most conventional air emission testing methods. With the significant potential benefits that the VISR method can bring, it is important to characterize and understand the precision and accuracy of this method.

Through a large number of tests under various process and environmental conditions, a high precision and accuracy have been demonstrated for the VISR method. The relative standard deviation (RSD) is in the range of 0.07-1.98% with an average RSD of 0.62% for flare CE in the range from 80 to 100%. The average RSD of 0.62% is more than an order of magnitude smaller than the minimum precision target of 20% RSD set in EPA Method 301. The highest SD is only 1.84 measured as % CE.

The flare CE measured by the VISR method is in excellent agreement with the flare CE measured by the extractive method. The mean difference between the two methods is in the range of -0.21 to 0.30 measured in % CE. The t-statistic value in each of the three test groups are well below its corresponding t-test critical value, passing the t-test with a substantial margin. Keep in mind that the extractive method is suitable only in research. It is virtually impossible to deploy the extractive method to elevated flares at industrial production facilities. Having a method that can be easily deployed to industrial sites and produce highly time-resolved and accurate flare measurement results is a significant advancement.

REFERENCES

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3. ENVIRON, Cost Analysis of HRVOC Controls on Polymer Plants and Flares, Report prepared for Texas Commission on Environmental Quality, Project 2008-104, Work Order 582-07-84005-FY08-12, 2008. http://www.tceq.state.tx.us/assets/public/implementation/air/rules/Flare/HRVOC_Cost_Analysis_Report.pdf (accessed March 23, 2015).
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5. Zeng, Y, J. Morris, and M. Dombrowski, Validation of a New Method for Measuring and Continuously Monitoring the Efficiency of Industrial Flares, *J. Air & Waste Manage. Assoc.* 66:76-86 (2016).
6. U.S. EPA, *Code of Federal Regulations*, Title 40, Part 63, Appendix A, Method 301, 2018.