

PROPOSAL

PVC REACTOR RELIEF TEST RUN

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DTH 000069720

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PVC REACTOR RELIEF TEST RUN

Proposal

R&D are requested to test the adequacy of Conoco's simulation of PVC reactor relief systems.

History

The existing Conoco PVC reactor relief system consists of two "Q" orifice relief valves (11.05 square inch relief area each) and an eight-inch double rupture disc (50.2 square inch area) vented to the atmosphere. It is planned to replace the double rupture disc systems with relief valves since the rupture discs can (and have) fail prematurely, resulting in unnecessary atmospheric emissions.

The expansion reactors at both Oklahoma City and Aberdeen are being built with only relief valve protection. Budget designs (totaling \$910,000) to modify the existing reactors have been prepared.

To design these systems, PED have recently simulated the reactor relief system. This simulation is complex, involving nonisothermal polymerization kinetics, multiphase, flashing critical flow while working with existing API equations for relief device capacity.

Finally, Conoco's reactor relief area for existing reactors is less than 50 percent of the recommended relief area for an FIA 1970 report and is thought to be less than several other manufacturers.

Proposed Test Run Description

The test run should accomplish the following:

1. Allow comparison of our nonisothermal kinetics model to actual data during runaway conditions.
2. Allow comparison of our critical flow relief valve capacity model to actual data, including both relief valves and equivalent orifices.
3. Allow comparison of our homogeneous, two-phase flow model to actual data giving pressure drop across rupture discs and entrance and exit effects.

The fifty-gallon reactor will be required for this test to provide sufficient reaction mass for scaleup. This test run will require venting VCM to the atmosphere (approximately 130 pounds per run). To minimize the possibility of personnel exposure, the test should be done on the weekend and during favorable weather conditions. It is our understanding that, because of the size of the test, no EPA report is required.

Proposed Test Run Description (Continued)

A proposed schedule of runs is given in Table I.

Data collected should include the following:

Pressure - Reactor
 - Inlet of Relief Valve or Orifice
 - Exit of Relief Valve or Orifice
 - Near End of Relief Header

Temperature - Reactor
 - Exit of Relief Valve or Orifice

Since the total relief is expected to last less than two minutes, high speed pressure and temperature measurements are needed. CED have indicated that they have a high speed multitrack tape recorder and some high speed pressure transmitters available.

It is also recommended that the atmospheric relief be recorded on film. This may allow for a qualitative analysis of relief system dynamics.

It should also be considered to sample air downwind of the release to analyze for flammability.

Note that the design calls for the use of the existing rupture disc or a manual vent for a backup method of overpressure control.

TABLE I

LIST OF RUNS

PVC REACTOR RELIEF TEST RUN

A. 1 1/2"-F-2" Relief Valve

The run is to check the accuracy of the simulation and to calibrate the high speed instruments.

B. 1"-E-2" Relief Valve

The run simulates the proposed reactor relief system.

C. "E" Size Orifice

The orifice is to be placed after the rupture disc. The run is to determine the difference in flows between relief valves and orifices of the same size.

D. 1 1/2", Schedule 40 Pipe

The 3.5-foot long pipe is to be connected to a header leading out of the building. This run is to simulate a double disc system.

The above runs should be done using conditions for 5385 resin. Cooling and agitation should be stopped at about 30 percent conversion. An additional run should be done using 5465 resin conditions, as this should produce higher pressures. Also, higher and perhaps lower conversions should be tried to confirm the simulation's results. Additional runs should be done using the "E" orifice relief valve system.

A total of at least six runs is, therefore, requested.

SIMULATION RESULTS

PVC REACTOR RELIEF TEST RUN

<u>Relief System</u>	MAXIMUM REACTOR PRESSURE, PSIG			
	<u>Conversion(1)</u>			
	<u>10%</u>	<u>30%</u>	<u>50%</u>	<u>70%</u>
"F" Relief Valve	203	203	202	201
"E" Relief Valve	210	208	207	203
"E" Orifice	207	216	225	207
1 1/2", Schedule 40 Pipe	203	-	-	-

(1) Values given are the polymerization conversion when the cooling water fails.

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SIMULATION BASIS

PVC REACTOR RELIEF TEST RUN

VCM Charge, Pounds	148
Water:Monomer Ratio	1.4:1
Catalyst	L-223
Catalyst Charge, Pounds	0.5(1)
Run Temperature, °F	134

<u>Relief System</u>	RELIEF SYSTEM DESCRIPTION(2)		
	<u>RV</u> <u>Area,</u> <u>Sq In</u>	<u>RD Set</u> <u>Point</u> <u>psig</u>	<u>RV Set</u> <u>Point</u> <u>psig</u>
"F" Relief Valve	0.307	200	190
"E" Relief Valve	0.196	200	190
"E" Orifice	0.196	200	-
1 1/2", Schedule 40 Pipe	-	200	-

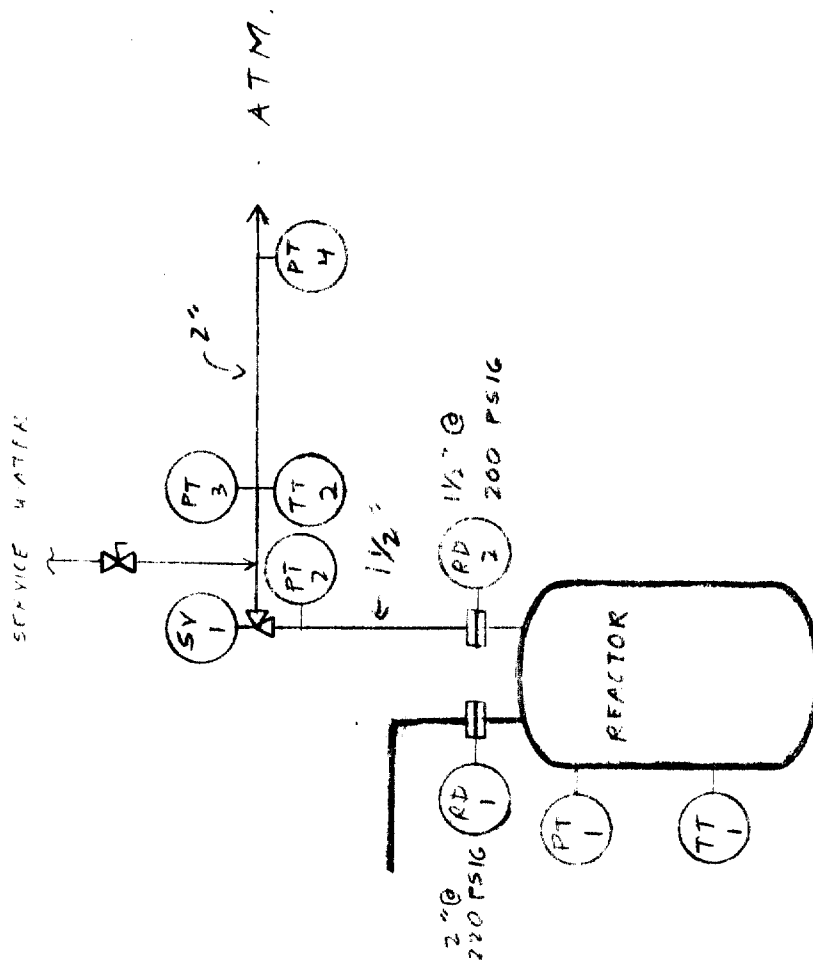
(1) Polymerization time to 80 percent is 365 minutes.

(2) All systems use 1 1/2-inch inlet and two-inch outlet pipes.

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PVC REACTOR RELIEF TEST RUN SCHEMATIC



— NEW
— EXISTING

BY M.S.W.

NOTES ON 2 OF 2

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NOTES FOR SCHEMATIC DIAGRAM

1. Not all details of existing equipment are shown.
2. SV-1 is on the existing 1 1/2-inch flange.
3. RD-1 replaces the existing two-inch RD at 200 psig.
4. PT-2 is to be as close to SV-1 as possible.
5. All PT's are quartz pressure transducers using a 1/2-inch screwed connection.
6. PT-1 and TT-1 may be replaced with existing instruments if their response speed is adequate.
7. PT-3 is to be as close to SV-1 as possible.
8. TT-3 is to be as close to PT-3 as possible.
9. PT-4 is to be close to the end of the pipe.
10. RD-1 may be replaced with a remote-operated valve.
11. All TT's are fine wire thermocouples.
12. SV-1 is E or F orifice, depending on the run.
13. All signals from PT's and TT's go to multitrack tape recorder Z-1.
14. SV-1 outlet piping is new.

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INSTRUMENT LIST
PVC REACTOR RELIEF TEST RUN

<u>Item No.</u>	<u>Service</u>
<u>Pressure Instruments</u>	
PT-1	Reactor Pressure
PT-2	Relief Valve Inlet Pressure
PT-3	Relief Valve Outlet Pressure
PT-4	End of Vent Pipe Pressure
<u>Temperature Transmitters</u>	
TT-1	Reactor Temperature
TT-2	Relief Valve Outlet Temperature
<u>Rupture Discs</u>	
RD-1	Reactor Emergency Relief
RD-2	Reactor Relief for Test
<u>Safety Valve</u>	
SV-1	Reactor Relief for Test
<u>Other Instruments</u>	
Z-1	High Speed Multitrack Recorder for Instruments
Z-2	High Speed Movie Camera for Velocity and Quality Measurements
Z-3 (Optional)	Accelorometer for Measurement of Shock Wave Velocity



Continental Oil Company
Engineering Center
Ponca City, Oklahoma
Pressure Instruments

SPECIFICATION SHEET

PROJECT NO. _____

A.F.E. NO. _____

DATE 9/26/80 INQ. NO. _____MADE BY MSW REQ. NO. _____APP'D. BY LLS P.O. NO. _____PLANT POHCA CITY PROJECT PVC REACTION RELIEF TEST KVN

1	TAG NO	<u>PT-1 THRU 4</u>							
2	SERVICE								
3									
4	INSTRUMENT TYPE	<u>PRESSURE TRANSM.</u>							
5	LOCATION	<u>(1)</u>							
6	RANGE, PSIG	<u>0-220 (2)</u>							
7	ELEMENT	<u>(3)</u>							
8	TYPE	MATERIAL							
9	LOCATION								
10	TEMPERATURE °F								
11	PRESSURE PSIG								
12	VALVE TYPE								
13									
14	LOCATION								
15	MATERIAL								
16	BODY SIZE	PORT SIZE							
17	PLUG FORM								
18	ΔP	MIN.	NOR.	MAX.					
19	CALC. Cv	VALVE Cv							
20	AIR TO OPEN OR CLOSE								
21	MAX SHUTOFF ΔP								
22	FLUID	<u>VCM-PVC SLURRY</u>							
23	TEMPERATURE °F	<u>200</u>							
24	PRESSURE PSIG	<u>MAX 220 (2)</u>							
25	API (M.W.)								
26	SP. GR. AT STD COND.								
27	SP. GR. AT P & T	<u>1.4</u>							
28	WEIGHT % VAPOR IN-OUT	<u>MAX 45 %</u>							
29	VISCOSITY AT P & T								
30	RATE, NORMAL								
31	RATE	MAX.	MIN. LB/SEC	<u>3</u>	<u>0</u>				
32	NOTES								

(1) SEE SCHEMATIC DIAGRAM

(2) MAXIMUM MAY NEED TO BE GREATER
TO ALLOW FOR SHOCK WAVE EFFECTS.
(3) TO BE DETERMINED.

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SHEET 1 OF 1 REV. _____



ENGINEERING CENTER

PONCA CITY OKLAHOMA
SPECIFICATION SHEET
TEMPERATURE INSTRUMENTS

A F F NO _____
DATE 9/26/80 W O NO _____
MADE BY MSW INQ NO _____
APP'D BY JRS REQ NO _____
B M NO _____ P O NO _____

PLANT PONCA CITY A.P.D. PROJECT PVC REACTOR RELIEF TEST RUN

1	TAG NO.	TT-1 / TT-2							
2	SERVICE								
3									
4	INSTRUMENT TYPE	TEMP TRANS							
5	LOCATION	(1)							
6	RANGE °F	0-200							
7	ELEMENT TYPE	(2)							
8	LOCATION								
9	TEMPERATURE °F								
10	PRESSURE PSIG								
11	VALVE TYPE								
12									
13	LOCATION								
14	MATERIAL								
15	BODY SIZE	PORT SIZE							
16	PLUG FORM								
17	ΔP	MIN.	NOR	MAX.					
18	CALC. CV	VALVE CV							
19	AIR TO OPEN OR CLOSE								
20	MAX SHUTOFF ΔP								
21	FLUID	VCM- PVC SLURRY							
22	TEMPERATURE °F	MAX	200						
23	PRESSURE PSIG	MAX	220 (2)						
24	°API (M. W.)								
25	SP. GR. AT STD. COND.								
26	SP. GR. AT P. & T.	1.4							
27	WEIGHT % VAPOR IN-OUT	MAX 45%							
28	VISCOSITY AT P & T								
29	RATE, NORMAL								
30	RATE	LB/SEC							
31	MAX	MIN	3	0					
32	NOTES:								

(1) SEE SCHEMATIC DIAGRAM

(2) TO BE DETERMINED

(3) PRESSURE MAY EXCEED 220 PSIG
DUE TO THE SHOCK WAVE.

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SHEET 1 OF 1 REV



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 PONCA CITY, OKLAHOMA
 SPECIFICATION SHEET

 A.F.E. NO. _____
 DATE 9/26 D.W.O. NO. _____
 MADE BY MSW I.N.O. NO. _____
 APP'D BY WPK REQ. NO. _____
 B.M. NO. _____ P.O. NO. _____

 PLANT PONCA CITY RYD PROJECT PVC REACTOR RELIEF TEST RUN

 ITEM NO. RD-1 AND RD-2
 SERVICE

RD-1

RD-2

DESCRIPTION

SINGLE DISC ASSEMBLY

CONNECTIONS

TWO INCH

ONE AND ONE-HALF INCH

300-POUND RF

300-POUND RF

HOLDER

EXISTING

SRB-7RS SAFETY HEAD (1)

WITH PRESSURE GAUGE

AND CHECK VALVE

316 SS INSERT TYPE

DISC MATERIAL

NICKEL

BURST PRESSURE

220 PSIG

200 PSIG

BURST TEMPERATURE

200°F

170°F

FLUID

PVC - VCM - H₂O

(1) EQUIVALENT

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SPECIFICATION SHEET

RELIEF VALVES

A.F.E. NO. _____

DATE 9/26/80

W O NO. _____

MADE BY M. J. C.

ING. NO. _____

APP'D BY WDE

REQ. NO. _____

B M NO. _____

P O NO. _____

PLANT SO GAC ACAI TOA PROJECT RELIEFTEST RUN

GENERAL							
1	ITEM NO. & TAG	SY-1		SY-1			
2	RELIEVES EQUIPMENT NO.						
3	MANUFACTURER	CONSOLIDATED		CONSOLIDATED			
4	MODEL NO.	1905-30Fc		1905-30Ec			
5		(1)		(1)			
SERVICE CONDITIONS							
6	FLUID	VCM-H ₂ O-PVC		VCM-H ₂ O-PVC			
7	STATE	FLASHING		SLURRY			
8	REQUIRED CAPACITY						
9	MOL. WT.						
10	SP. GR.						
11	VISCOSITY						
12	COMPRESSIBILITY FACTOR						
13	DESIGN PRESS. OF EQUIPMENT						
14	PRESS. OPERATING						
15	RELIEVING						
16	TEMP. FLOWING						
17	RELIEVING						
18	BACK PRESSURE	SC		SC			
19	DIFFERENTIAL SET PRESSURE						
20	ACCUMULATION %						
21	BLOW DOWN %						
22							
BASIS OF SELECTION							
23	CODE REQUIREMENT						
24	EXPOSED AREA						
25	FIRE INSULATION THICKNESS						
26	OTHER BASIS						
DESIGN DETAILS							
27	DESIGN TYPE	BELLLOUS		BELLLOUS			
28	SEAT TYPE						
29	BONNET (OPEN OR CLOSED)	OPEN		OPEN			
30	INLET SIZE RATING, FACING	1 1/2" - 150 RF		1" - 150 RF			
31	OUTLET SIZE, RATING, FACING	1" - 150 RF		2" - 150 RF			
32	CALCULATED AREA						
33	ORIFICE LETTER	F		E			
34	ACTUAL AREA	0.707		.196			
MATERIALS							
35	BODY	CS		CS			
36	BONNET	CS		CS			
37	SEAT & DISK	SS		SS			
38	GUIDE & RING	SS		SS			
39	SPRING	CS		CS			
40	BELLOWS	SS		SS			
ACCESSORIES							
41	LIFTING LEVER (PLAIN OR PACKED)	NO		NO			
42	GAG	NO		NO			
43	CODE STAMP						
44	CAP (SCREWED OR BOLTED)						
45	OTHER						

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NOTES:

(1) OF EQUIVALENT

MANUFACTURER SHALL VERIFY SELECTION OF ORIFICE SIZE AND MATERIALS.

VALVES SHALL MEET DIMENSION REQUIREMENTS OF API RP-526.

VALVES SHALL MEET TEST REQUIREMENTS OF API RP-527.

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SUPPLIER TO COMPLETE FORM BY FURNISHING
INFORMATION FOR BLANK SPACES

SHEET _____ OF _____ REV. _____



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SPECIFICATION SHEET

ORIFICE PLATES & FLANGES

INCLUDING DATA FOR BORE CALCULATION

A.F.E. NO.

DATE 9/26/80

W.O. NO.

MADE BY MSA

INO. NO.

APP'D BY WRS

REQ. NO.

B.M. NO.

P.O. NO.

PLANT 50 GAL REACTOR PROJECT REACTOR RELIEF TEST RUN

GENERAL SPECIFICATION						
1						
2	ORIFICE PLATES			9	ORIFICE FLANGES	
3	MAKE TO AGA-ASME STANDARD		OTHER	10	RATING & FACING	
4	PLATE MATERIAL	316S.S.	OTHER	11	TYPE	WELD NECK
5	RTJ RING MAT'L & TYPE			12	MAT'L	STEEL
6	BORE MAXIMUM RATE		NEAREST 1/8"	13	TAP SIZE	1/2" NPT
7	STAMP TO ISA STANDARD		OTHER	14	FLANGES BY	
8						15
16	TAG NO.		OR-1			
17	LINE NO.					
18						
19	SERVICE CONDITIONS					
20	FLUID YCM-FY-1120					
21	FLOW UNITS LB/SEC					
22	MAXIMUM FLOW 7					
23	NORMAL FLOW -					
24	FLOW PRESSURE PSIG 220 (1)					
25	FLOW TEMPERATURE °F 200					
26	S. G. @ 60°F &		PSIA			
27	S. G. @ F. T. &		PSIA	1.1		
28	SUPERCOMP. FACTOR @ O. P.					
29	VAPOR GAS MOL WT 0.605					
30	VISCOSITY, CP @ F. T.					
31	STEAM QUALITY, %					
32	STEAM SUPERHEAT °F					
33						
34						
35						
36						
37						
38						
39						
40						
41						
42	MEASURING STATION DATA					
43	ACTUAL ORIFICE I. D., INS.		0.4996			
44	LINE FLANGE I. D., INS.		2			
45	SEAL S. G. @ 60°F					
46	MANOMETER TYPE					
47	DIFF. RANGE INS H ₂ O DRY					
48	STATIC RANGE, PSIA					
49	CHART OR SCALE RANGE					
50	CHART MULTIPLIER					
51						
52						
53						
54						
55						
56						
57						
58						
59	DTH 000069734					

NOTES: (1) PRESSURE MAY EXCEED THIS FIGURE
DUE TO SHOCK WAVES

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INSTRUMENT SOCIETY OF AMERICA

SHEET 1 OF 1 REV



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SPECIFICATION SHEET

A.F.E. NO. _____
DATE 9/26/80 W.O. NO. _____
MADE BY MSW INQ. NO. _____
APP'D BY WRF REQ. NO. _____
B.M. NO. _____ P.O. NO. _____

PLANT CYL REACTOR PROJECT REACTOR RELIEF TEST RUN

ITEM NO 2-1
SERVICE HIGH SPEED MULTI-TRACK RECORDED

TO BE CONNECTED TO PT-1 THRU PT-4
AND TT-1 AND TT-2. THIS WILL
ALLOW LATER ANALYSIS OF THE
TEST RUNS. 2-3 MAY ALSO BE
CONNECTED. REQUIREMENTS TO BE
SET BY CED.

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SHEET 1 OF 1 REV _____