

where

- D_t = theoretical draft intensity created by pressure transformer, inches of water.
 h_f = draft loss due to friction in pressure transformer, inches of water.
 h_F = draft loss through the fuel bed, inches of water.
 h_B = draft loss through the boiler and setting, inches of water.
 h_{Br} = draft loss through the breeching, inches of water.
 h_v = draft loss due to velocity, inches of water.
 h_{Bd} = draft loss due to bends, inches of water.
 h_C = draft loss due to contraction of opening, inches of water.
 h_O = draft loss due to enlargement of opening, inches of water.
 h_E = draft loss through the economizer, inches of water.
 h_R = draft loss through recuperators and regenerators, inches of water.

The left hand member of Equation 13 represents the total amount of available draft created by the pressure transformer, that is, the natural draft chimney, Venturi chimney, or fan, and is equal to the theoretical intensity less the internal losses incidental to operation. The right hand member represents the sum of all of the various losses of draft throughout the entire boiler plant installation outside of the pressure transformer itself. The left hand member expresses the available intensity and is

TABLE 1. RECOMMENDED MINIMUM CHIMNEY SIZES FOR HEATING BOILERS AND FURNACES†

WARM AIR FURNACE CAPACITY IN SQ. IN. OF LEADER PIPE	STEAM BOILER CAPACITY SQ. FT. OF RADIATION	HOT WATER HEATER CAPACITY SQ. FT. OF RADIATION	NOMINAL DIMENSIONS OF FIRE CLAY LINING IN INCHES	RECTANGULAR FLUE		ROUND FLUE		HEIGHT IN FT. ABOVE GRATE
				Actual Inside Dimensions of Fire Clay Lining in Inches	Actual Area Sq. In.	Inside Diameter of Lining in Inches	Actual Area Sq. In.	
790	590	973	8½ x 13	7 x 11½	81			35
1000	690	1,140				10	79	
	900	1,490	13 x 13	11¼ x 11¼	127			40
	900	1,490	8½ x 18	6¾ x 16¼	110	12	113	
	1,100	1,820				15	177	
	1,700	2,800	13 x 18	11¼ x 16¼	183			45
	1,940	3,200				18	254	50
	2,130	3,520	18 x 18	15¾ x 15¾	248	20	314	
	2,480	4,090	20 x 20	17¼ x 17¼	298			55
	3,150	5,200				22	380	60
	4,300	7,100				24	452	65
	4,600	7,590	20 x 24	17 x 21	357			
	5,000	8,250	24 x 24	21 x 21	441			
	5,570	9,190		24 x 24*	576			
	5,580	9,200				22	380	
	6,980	11,500				24	452	
	7,270	12,000		24 x 28*	672			
	8,700	14,400		28 x 28*	784			
	9,380	15,500				27	573	
	10,150	16,750		30 x 30*	900			
	10,470	17,250		28 x 32*	896			

*Dimensions are for unlined rectangular flues.

†This table is taken from the A.S.H.V.E. Code of Minimum Requirements for the Heating and Ventilation of Buildings (Edition of 1929).

analogous to the head developed by a centrifugal pump in a water works system while the right hand member expresses the required draft intensity and is analogous to the total dynamic head in a water works system. For a general circulation of gases, then

$$D_a = D_r \quad (14)$$

where

D_a = available draft intensity, inches of water.

D_r = required draft, inches of water.

The draft loss through the fuel bed (h_F) or the amount of draft required to effect a given or required rate of combustion, varies between wide limits and represents the greater portion of the required draft. In coal-fired

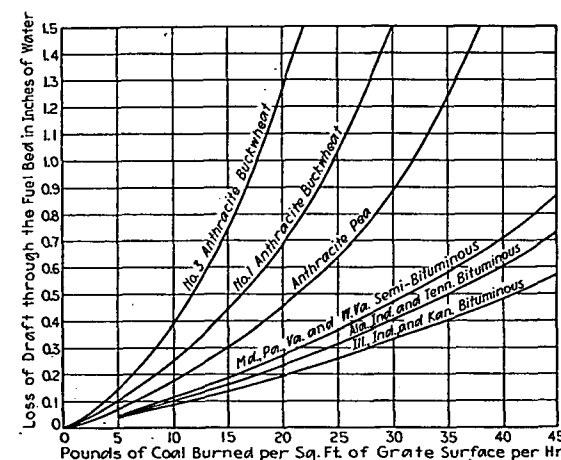


FIG. 8. DRAFT REQUIRED AT DIFFERENT RATES OF COMBUSTION FOR VARIOUS KINDS OF COAL

installations, the draft loss through the fuel bed is dependent upon the following factors:

1. Character and condition of the fuel, clean or dirty.
2. Percentage of ash in the fuel.
3. Volume of interstices in the fuel bed, coarseness of fuel.
4. Thickness of the fuel bed, rate of combustion.
5. Type of grate or stoker used.
6. Efficiency of combustion.

There is a certain intensity of draft with which the best results will be obtained for every kind of coal and rate of combustion. Fig. 8 gives the intensity of draft, or the vacuum in the combustion chamber required to burn various kinds of coal at various rates of combustion. Expressed in other words, these curves represent the amount of draft required to force the necessary amount of air through the fuel bed in order to effect various