

different from those in factories, since there must be a considerable volume of air circulated in order to provide ventilation and cooling.

COOLING LOAD

The cooling load may be divided into the following parts:

1. Transmission of heat through walls, roof, glass, etc., with allowances for sun-exposed surfaces and heat capacity.
2. Transmission of solar radiation through glass and absorption by interior furnishings.
3. Heat and moisture from infiltration and from outside air introduced.
4. Heat and moisture from occupants and heat from lights, machinery and other sources.

Transmission With No Sun Effect

The transmission load *for surfaces not exposed to the sun* is calculated in a manner similar to that described in Chapter 7, by means of the following formula:

$$H_t = A U (t_o - t) \quad (1)$$

where:

H_t = heat transmitted through the material of the wall, glass, roof, or floor in Btu per hour.

A = net inside area of wall, glass, roof, or floor in square feet.

t = inside temperature, degrees Fahrenheit.

t_o = outside temperature, degrees Fahrenheit.

U = coefficient of transmission of wall, floor, roof, or glass in Btu per hour per square foot per degree Fahrenheit difference in temperature. (Tables 8 to 18, Chapter 5).

Temperatures

The maximum cooling load in summer may be calculated for an outside dry-bulb temperature not to exceed 95 F and a wet-bulb temperature not to exceed 80 F. While higher outside dry-bulb temperatures are frequently observed they are either of short duration or accompanied by low relative humidities. Weather Bureau reports are frequently misleading in this respect as they report the maximum temperature for the day with the relative humidity which occurs during a different period and which usually is much higher than the relative humidity occurring at the maximum temperature. Any statement of weather condition which gives a wet-bulb temperature higher than 80 F in the United States is questionable.

Summer dry-bulb and wet-bulb temperatures for various cities are given in Table 1. It will be noted that the wet-bulb temperatures are not the maximums but the design temperatures which should be used in air-conditioning calculations. The maximum outside wet-bulb temperatures as given in Weather Bureau reports usually occur only from 1 per cent to 4 per cent of the time, and they are therefore of such short duration that it is not practical to design a cooling system covering this range.

Sun Effect

Solar radiation is an important factor in the mechanism of heat flow into buildings. Research conducted at the A.S.H.V.E. Research Labora-

TABLE 1. AVERAGE MAXIMUM DESIGN DRY-BULB TEMPERATURES, DESIGN WET-BULB TEMPERATURES, WIND VELOCITIES, AND WIND DIRECTIONS FOR JUNE, JULY, AUGUST, AND SEPTEMBER

STATE	CITY	AVERAGE MAXIMUM DESIGN DRY-BULB	DESIGN WET-BULB	SUMMER WIND VELOCITY MPH	PREVAILING SUMMER WIND DIRECTION
Ala.	Birmingham	93	77	5.2	S
	Mobile	94	78	8.6	SW
Ariz.	Phoenix	110	77	6.0	W
Ark.	Little Rock	95	77	7.0	NE
Calif.	Los Angeles	88	70	6.0	SW
	San Francisco	85	68	11.0	SW
	San Francisco	90	64	6.8	S
Colo.	Denver	88	74	7.3	S
Conn.	New Haven	93	76	6.2	S
D. C.	Washington	94	78	8.7	SW
Fla.	Jacksonville	94	79	7.0	E
	Tampa	91	75	7.3	NW
Ga.	Atlanta	95	79	7.8	SW
	Savannah	95	65	5.8	NW
Idaho.	Boise	88	73	10.2	NE
Ill.	Chicago	91	75	8.2	S
	Peoria	90	73	9.0	SW
Ind.	Indianapolis	92	74	6.6	SW
Iowa.	Des Moines	94	75	8.0	SW
Ky.	Louisville	94	79	7.0	SW
La.	New Orleans	85	71	7.3	S
Maine.	Portland	93	76	6.9	SW
Md.	Baltimore	88	73	9.2	SW
Mass.	Boston	88	72	10.3	SW
Mich.	Detroit	84	72	8.4	SE
Minn.	Minneapolis	95	78	6.2	SW
Miss.	Vicksburg	92	75	9.5	S
Mo.	Kansas City	93	76	9.4	SW
	St. Louis	87	63	7.3	SW
Mont.	Helena	93	74	9.3	S
Nebr.	Lincoln	93	64	7.4	W
Nev.	Reno	93	75	10.0	SW
N. J.	Trenton	90	74	7.1	S
N. Y.	Albany	83	72	12.2	SW
	Buffalo	91	75	12.9	SW
	New York	87	63	6.5	SE
N. M.	Santa Fe	87	72	5.6	SE
N. C.	Asheville	93	79	7.8	SW
	Wilmington	88	69	8.8	NW
N. D.	Bismarck	87	72	9.9	S
Ohio.	Cleveland	93	75	6.6	SW
	Cincinnati	96	76	10.1	S
Okla.	Oklahoma City	83	65	6.6	NW
Ore.	Portland	93	76	9.7	SW
Pa.	Philadelphia	91	73	9.0	NW
	Pittsburgh	85	73	10.0	NW
R. I.	Providence	94	80	9.9	SW
S. C.	Charleston	93	76	6.8	NE
	Greenville	94	76	6.5	SW
Tenn.	Chattanooga	93	77	7.5	SW
	Memphis	93	77	7.5	SW