

Note that the ratio (space latent load/1076) is the equivalent of the required rate of water vapor removal in pounds per hour. If the rate of water removed is known, it may be used directly in Equation 18.

3. Draw a line through the reference point on the A.S.H.V.E. psychrometric chart and the value of $(h_i - h_s)/(W_i - W_s)$ determined above. Draw a second line through the state point of the room air (design wet-bulb and dry-bulb temperatures) parallel to this line. This is the *condition line* for the process.

4. Read the temperature where the condition line from step 3 intersects the saturation line. This is called the *apparatus dew point*.

See Fig. 5. Note that instead of using this graphical method the left hand side of Equation 18 may be solved by trial and error by substituting values of h , and W , corresponding to assumed apparatus dew-point temperatures.

5. Compute the required air quantity from the relation

$$Q_{ra} = \frac{(\text{Space sensible load})}{1.08 \left[\left(\frac{\text{Space}}{\text{dry-bulb}} \right) - \left(\frac{\text{Apparatus}}{\text{dew-point}} \right) \right] \times \left(1 - \frac{\text{Coil}}{\text{bypass factor}} \right)} \quad (19)$$

The magnitude of Q_{ra} is substantially the quantity, cfm, of cooled and dehumidified air for which the distribution system must be designed.

The numerical factor 1.08 is derived from the product $1 \text{ cfm} \times 60 \text{ min} \times 0.244 \times 0.075 \left(1 - \frac{0.00923}{0.62} \right) = 1.08$, assuming an average supply air dew point of 55 F. Since standard air density (0.075) includes the weight of the water vapor, it is desirable to reduce it to the basis of dry air by the last factor where $0.00923 =$ humidity ratio of air at 55 F dew point, and $0.62 =$ ratio of density of water vapor to dry air at same temperature and pressure. Refer to Chapter 36 for coil selection.

Note that the product [(space dry-bulb) - (apparatus dew point)] $\times$ (1 - coil bypass factor) is equal to the dry-bulb range through which the conditioned air is cooled. Hence, in rare instances when the *condition line* of the process may not intersect the saturation line, any other convenient reference temperature on the *condition line* may be used instead, provided that the coil bypass factor is specified accordingly on the proper basis.

MINIMUM ENTERING AIR TEMPERATURE

Due consideration must be given to the temperature of the air entering the conditioned space in order to prevent objectionable drafts. With ceiling type diffusers or wall grilles with a high aspect ratio (see Chapter 31), many engineers consider 20 deg as the maximum difference for good design under average conditions. This difference can only be exceeded with extremely high ceiling outlets or wall grilles. Thus, if 80 F dry-bulb is to be maintained in a space with average ceiling height, the minimum delivered air temperature would be limited to about 60 F dry-bulb temperature. If the latent heat load is relatively high, it is often necessary to circulate more air with a higher delivered dry-bulb temperature in order to produce a thermodynamic balance. If the dry-bulb temperature of the air supplied to the space is known, the required air quantity can be calculated from the formula,

$$Q_{ra} = \frac{q_s}{1.08 (t_i - t_s)} \quad (20)$$

or the supply temperature t_s can be determined as follows.

$$t_s = t_i - \frac{q_s}{1.08 \times Q_{ra}} \quad (21)$$

EXAMPLE—COOLING LOAD CALCULATION

Example 13: A one-story office building Fig. 6 is located in an eastern state near 40 deg latitude. The adjoining buildings on the north and west are not conditioned, and the air temperature within them is known to be substantially equal to the outdoor air temperature at any time of the day.

South wall construction: 8 in. concrete block, 4 in. brick veneer. (Table 7, Chapter 9, $U = 0.41$.)

East wall and outside north wall construction: 8 in. concrete block, no plaster on walls. (Table 6, Chapter 9, $U = 0.52$.)

West wall and adjoining north party wall construction: 13 in. solid brick, no plaster:

$$\frac{1}{U} = \frac{1}{1.65} + \frac{13}{5} + \frac{1}{1.65} \quad \text{or,} \quad U = 0.263. \quad \text{Use } U = 0.26.$$

Roof construction: $2\frac{1}{2}$ in. flat roof deck of 2 in. gypsum slab on $\frac{1}{4}$ in. asbestos cement board surfaced with built-up roofing. (Table 13B, $U = 0.34$ for summer.)

Floor construction: 4 in. concrete on ground.

Window: 3 ft x 5 ft, non-opening type, with medium colored Venetian blinds for windows on south wall. Approximately 4 in. reveal on all windows.

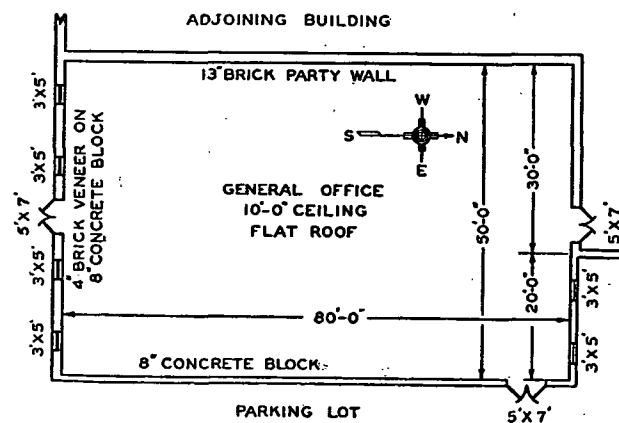


FIG. 6. PLAN OF ONE-STORY OFFICE BUILDING

Front doors: Two 2 ft-6 in. x 7 ft (glass panels).

Side doors: Two 2 ft-6 in. x 7 ft ($\frac{1}{2}$ glass panels).

Rear doors: Two 2 ft-6 in. x 7 ft (wood panels).

Outside design conditions: Maximum dry-bulb 95 F, wet-bulb 78 F; $W_o = 0.0169$ lbs vapor per lb dry air; $h_o = 41.38$ Btu per lb dry air.

Indoor design conditions: Dry-bulb 80 F, wet-bulb 65 F; $W_i = 0.0098$ lb vapor per lb dry air; $h_i = 29.95$ Btu per lb dry air.

Occupancy: 85 office workers.

Lights: 12,000 watts, fluorescent; 4000 watts tungsten.

Fan motor: $7\frac{1}{2}$ hp.

Assume that cooling coil has a bypass factor of 0.15, i.e., that 15 percent of the air passes through the coil without contacting the coil surface.

Conditioning equipment to be located in adjoining structure to north.

Find: Total, sensible, and latent maximum cooling loads and required air quantity through conditioning equipment.