

effective temperature for sedentary persons, as determined at the A.S.H.V.E. Research Laboratory, is 66 deg.

According to Fig. 6, Chapter 2, for so-called still air conditions, a relative humidity of approximately 50 per cent is required to produce an effective temperature of 66 deg when the dry-bulb temperature is 70 F. However, even where provision is made for artificial humidification, the relative humidity is seldom maintained higher than 40 per cent during the extremely cold weather, and where no provision is made for humidification, the relative humidity may be 20 per cent or less. Consequently, in using the figures listed in Table 1, consideration should be given to whether provision is to be made for humidification, and if so, the actual relative humidity to be maintained.

TABLE 1. WINTER INSIDE DRY-BULB TEMPERATURES USUALLY SPECIFIED^a

TYPE OF BUILDING	DEG FAHR	TYPE OF BUILDING	DEG FAHR
SCHOOLS—		THEATERS—	
Class rooms.....	70-72	Seating space.....	68-72
Assembly rooms.....	68-72	Lounge rooms.....	68-72
Gymnasiums.....	55-65	Toilets.....	68
Toilets and baths.....	70		
Wardrobe and locker rooms.....	65-68	HOTELS—	
Kitchens.....	66	Bedrooms and baths.....	70
Dining and lunch rooms.....	65-70	Dining rooms.....	70
Playrooms.....	60-65	Kitchens and laundries.....	66
Natatoriums.....	75	Ballrooms.....	65-68
		Toilets and service rooms.....	68
HOSPITALS—		HOMES.....	70-72
Private rooms.....	70-72	STORES.....	65-68
Private rooms (surgical).....	70-80	PUBLIC BUILDINGS.....	68-72
Operating rooms.....	70-95	WARM AIR BATHS.....	120
Wards.....	68	STEAM BATHS.....	110
Kitchens and laundries.....	66	FACTORIES AND MACHINE SHOPS.....	60-65
Toilets.....	68	FOUNDRIES AND BOILER SHOPS.....	50-60
Bathrooms.....	70-80	PAINT SHOPS.....	80

^aThe most comfortable dry-bulb temperature to be maintained depends on the relative humidity and air motion. These three factors considered together constitute what is termed the *effective temperature*. (See Chapter 2.)

Temperature at Proper Level: In making the actual heat loss computations, however, for the various rooms in a building it is often necessary to modify the temperatures given in Table 1 so that the air temperature at the proper level will be used. By *air temperature at the proper level* is meant, in the case of walls, the air temperature at the mean height between floor and ceiling; in the case of glass, the air temperature at the mean height of the glass; in the case of roof or ceiling, the air temperature at the mean height of the roof or ceiling above the floor of the heated room; and in the case of floors, the air temperature at the floor level.

High Ceilings: Research data concerning stratification of air in buildings are lacking, but in general it may be said that where the increase in temperature is due to the natural tendency of the warmer or less dense air to rise, as where a direct radiation system is installed, the temperature

of the air at the ceiling increases with the ceiling height. The relation, however, is not a straight line function, as the amount of increase per foot of height apparently decreases as the height of the ceiling increases, according to present available information¹.

Where ceiling heights are under 20 ft, it is common engineering practice to consider that the Fahrenheit temperature increases 2 per cent for each foot of height above the breathing line. This rule, sufficiently accurate for most cases, will give the probable air temperature at any given level for a room heated by direct radiation. Thus, the probable temperature in a room at a point 3 ft above the breathing line, if the breathing line temperature is 70 F, will be $[1.00 + (3 \times 0.02)] 70 = 74.2$ F.

With certain types of heating and ventilating systems, which tend to oppose the natural tendency of warm air to rise, the temperature differential between floor and ceiling can be greatly reduced. These include fan-furnace heaters, unit heaters, and the various types of mechanical ventilating systems. The amount of reduction is problematical in certain instances, as it depends upon many factors such as location of air outlets, the incoming air temperature, and direction and velocity of the air discharge. In some cases it has been possible to reduce the temperature between the floor and ceiling by a few degrees, whereas, in other cases, the temperature at the ceiling has actually been increased because of improper design, installation or operation of equipment. So much depends upon the factors enumerated that it is not advisable to allow less than 1 per cent per foot (and usually more) above the breathing line in arriving at the air temperature at any given level for any of these types of heating and ventilating systems, unless the manufacturers are willing to guarantee that the particular type of equipment under consideration will maintain a smaller temperature differential for the specific conditions involved.

OUTSIDE TEMPERATURES

The outside temperature used in computing the heat loss from a building is seldom taken as the lowest temperature ever recorded in a given locality. Such temperatures are usually of short duration and are rarely repeated in successive years. It is therefore evident that a temperature somewhat higher than the lowest on record may be properly assumed in making the heat loss computations.

The outside temperature to be assumed in the design of any heating system is ordinarily not more than 15 F above the lowest recorded temperature as reported by the Weather Bureau during the preceding 10 years for the locality in which the heating system is to be installed. In the case of massive and well insulated buildings in localities where the minimum does not prevail for more than a few hours, or where the lowest recorded temperature is extremely unusual, more than 15 F above the minimum may be allowed, due primarily to the *fly-wheel effect* of the heat capacity of the structure. Table 2 lists the coldest dry-bulb temperatures ever recorded by the Weather Bureau at the places listed. Recommended design temperatures are given in Fig. 1.

¹A.S.H.V.E. RESEARCH REPORT No. 958—Temperature Gradient Observations in a Large Heated Space, by G. L. Larson, D. W. Nelson and O. C. Cromer (A.S.H.V.E. TRANSACTIONS, Vol. 39, 1933, p. 243). A.S.H.V.E. RESEARCH REPORT No. 1011—Tests of Three Heating Systems in an Industrial Type of Building, by G. L. Larson, D. W. Nelson and John James (A.S.H.V.E. TRANSACTIONS, Vol. 41, 1935, p. 185).